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# 3 Prosthetics, Neural

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## 5 Introduction

6 This article provides an overview of the physical components that  
7 tend to be common to all neural prosthetic systems. It emphasizes  
8 the biophysical factors that constrain the sophistication of those  
9 interfaces. Specific applications to neural prosthetic systems for  
10 sensory replacement and motor control are covered in PROSTHET-  
11 ICS, SENSORY SYSTEMS and PROSTHETICS, MOTOR CONTROL, re-  
12 spectively. Electrical stimulation of the nervous system is also be-  
13 ing used to treat other disorders; examples include spinal cord  
14 stimulation to control pain and basal ganglia stimulation to control  
15 parkinsonian dyskinesias.

## 16 Electroneural Interfaces

17 Two types of physical system are known to be capable of real-time  
18 information processing: electronic circuits, in which information is  
19 carried by the flow of electrons in metal conductors, and neural  
20 circuits, in which information is carried by ions in water. Much  
21 contemporary research in computational neurobiology is concerned  
22 with discovering or exploiting common principles of information  
23 processing in these two systems. Thus, it is natural that real-time  
24 interfaces between these systems have been developed so that elec-  
25 tronic instrumentation can be used to study neural systems. Neural  
26 prosthetics are clinical applications of neural control interfaces  
27 whereby information may be exchanged between neural and elec-  
28 tronic circuits. Their technology to date has been derived largely  
29 from cardiac pacemakers, which themselves have evolved from the  
30 fixed-rate, single-channel stimulators of the 1950s to become pro-  
31 grammable and adaptive systems equipped with sensors and so-  
32 phisticated data processing.

33 In principle, information could be transferred into and out of the  
34 nervous system by any of several means, including chemical, mag-  
35 netic, optical, and ultrasonic. In practice, neural prostheses require  
36 temporospatial resolution and physical portability, which have only  
37 been achieved with the types of electrical signals that are familiar  
38 to most electrophysiologists. Thus, the future of neural prosthetics  
39 depends heavily on the well-understood biophysical properties of  
40 excitable membranes and on the development of technology that  
41 can approach physical limits that are readily predictable from those  
42 properties.

43 In addition to the obvious goal of restoring function to patients  
44 with disabilities, the field of neural prosthetics offers important  
45 opportunities for pure research:

- 46 • The clinical and commercial value of neural prostheses justifies  
47 the development of technology that is also useful in basic  
48 research.
- 49 • The implantation of sophisticated neural control interfaces in  
50 sentient observers creates unique opportunities for a new class  
51 of psychophysical research into neural computation.
- 52 • The development of functional replacement parts for the nervous  
53 system forces researchers to examine and test theories of neural  
54 computing more rigorously than they might do otherwise.
- 55 • The development of neural prosthetic controllers that can deal  
56 successfully with the exigencies of daily life will almost certainly  
57 require advancement of principles and methods for neural net-  
58 works and other forms of adaptive control.

## 60 Stimulation

61 Most neural prosthetic devices operate by injecting electrical cur-  
62 rent into the extracellular fluids surrounding excitable neurons in  
63 order to elicit action potentials in those neurons. Action potentials  
64 so elicited are indistinguishable from those that arise through the

65 natural mechanisms of sensory transduction or synaptic input.  
66 When these action potentials arrive at their destinations, the re-  
67 ceiving cells respond to and interpret the signals as if they arose  
68 from naturally occurring neural activity. Thus, the goal of the neu-  
69 ral prosthetic device is to recreate the temporospatial pattern of  
70 activity that would have occurred normally during the particular  
71 function that is being replaced or augmented prosthetically (see  
72 PROSTHETICS, SENSORY SYSTEMS, for a discussion of these factors  
73 in cochlear implants).

75 *Biophysics.* Topologically, a neuron in its resting state is essen-  
76 tially a charged spherical capacitor with elongated deformations  
77 comprising its axon and dendrites. The cell membrane is the di-  
78 electric, the ionic solutions on either side of the membrane consti-  
79 tute the plates, and differences in the concentrations of ions on each  
80 side generate the charging potential of about  $-70$  mV (inside ver-  
81 sus outside). In order to generate an action potential, the membrane  
82 capacitance must be discharged by about 15 mV in a small region.  
83 This results in a brief sequence of openings and closings of sodium  
84 and potassium channels in the membrane, which results in the flow  
85 of the action current. The action current depolarizes and then re-  
86 polarizes adjacent regions of the cell membrane, giving rise to the  
87 propagating wave of activity known as an action potential or spike.

88 The process of evoking an action potential through extracellular  
89 stimulation is somewhat counterintuitive. In order to depolarize a  
90 capacitor, it is necessary to pass charge across the dielectric, i.e.,  
91 into the cell body. However, neither the source nor the sink elec-  
92 trode of the stimulator is actually inside the cell. Instead, the stim-  
93 ulator creates a voltage gradient in the tissues surrounding the target  
94 cell. This gradient induces charge to flow across the cell membrane  
95 by capacitive conductance in response to the rate of change of the  
96 voltage gradient, i.e.,  $dV/dt$ . The amount and extent of the depo-  
97 larization so produced depend on the intensity and time course of  
98 the pulse of stimulation current, its propagation through the various  
99 conductances in the tissues through which it diffuses, and the phys-  
100 ical dimensions and consequent electrical properties of the excitable  
101 target cell (Ranck, 1975).

102 The most important physical dimension of highly elongated neu-  
103 rons is their diameter, which affects the ratio of membrane surface  
104 area (which determines capacitance) to axonal cross-sectional area  
105 (which determines resistance to current spread inside the cell). The  
106 presence, thickness, and disposition of myelin are also important  
107 because myelin greatly reduces the capacitance that must be dis-  
108 charged in order to reach threshold depolarization. It should also  
109 be remembered that electrical current must form a complete circuit,  
110 so that any capacitive stimulation current that enters a cell at one  
111 point, depolarizing its cell membrane locally, must be balanced by  
112 equal current leaving the cell and causing some degree of local  
113 hyperpolarization in other regions.

114 In order to predict accurately the effects of stimulating a complex  
115 structure such as a part of the cerebral cortex or a muscle with  
116 embedded sensory and motor axons, it is necessary to have a great  
117 deal of quantitative information about the neural architecture and  
118 the disposition of the stimulating electrodes. There are some useful  
119 rules of thumb, however, that cover most of the important  
120 phenomena:

- 121 • The most important consequence of a stimulation pulse is the  
122 steepness of the extracellular field gradient that it produces in the  
123 vicinity of the target neurons. Small electrodes positioned close  
124 to excitable processes are most effective.
- 125 • The important stimulus variable is the charge of a pulse, which  
126 is current times duration. Voltage is not important, as most of  
127 the voltage tends to be dissipated across the metal-electrolyte  
128 interface (see below) rather than contributing to the voltage gra-  
129 dient in the tissue surrounding the neurons.
- 130 • Stimulation pulses are most efficient when they have a duration  
131 that is somewhat shorter than the membrane time constant of the  
132 target cells, which is usually on the order of  $100\text{--}200\ \mu\text{s}$  for  
133 myelinated axons and  $500\text{--}1,000\ \mu\text{s}$  for unmyelinated axons and  
134 cell bodies.
- 135 • The first recruited elements tend to be the largest, most elongated,  
136 and most myelinated elements, namely large-diameter myeli-

137 nated axons and large cell bodies attached to myelinated axons.  
138 • Most body tissues (including bone and scar tissue) are suffi-  
139 ciently conductive that they tend, in aggregate, to act as volume  
140 conductors in which stimulus current density steadily decreases  
141 with distance from the electrode.  
142 • Stimulation electrodes must be used in pairs (source and sink),  
143 but each contact tends to function as an independent monopolar  
144 electrode unless the two contacts are positioned closer together  
145 than the target neurons.

147  
148 *Electrochemistry.* The rise of safe and effective neural prosthetic  
149 devices over the past 30 years is a consequence of the gradual  
150 elucidation of the electrochemical processes involved in converting  
151 electrical current from flow of electrons in a metal conductor to  
152 flow of ions in an aqueous one. In order for this to occur without  
153 cumulative deterioration of the electrodes or damage to the tissues,  
154 it is necessary that this be accomplished by entirely reversible  
155 chemical reactions. The typical reactions of electrolysis result in  
156 irreversible breakdown of water molecules into gases and acid or  
157 alkali solutions and shifts of the neutral valence of metals into  
158 positive-valence oxides with very different electrical, chemical, and  
159 biotoxic properties (reviewed by Loeb, McHardy, and Kelliher,  
160 1982).

161 The most obvious fully reversible reaction is the charging and  
162 discharging of the capacitance between the metal electrode and the  
163 body fluids. Because the irreversible reactions of electrolysis all  
164 have minimal working voltages that must be exceeded before they  
165 occur (usually about  $\pm 0.8$  VDC), stimulating current can be passed  
166 into and out of the electrode safely as long as capacitive charging  
167 never reaches these working voltages. Thus, repeated brief pulses  
168 of electrical current can be applied safely, as long as an equal and  
169 opposite amount of charge flows in the opposite direction between  
170 each stimulating pulse.

171 The amount of charge that can be passed by this double-layer  
172 charging depends on the capacitance of this interface, which de-  
173 pends on the surface area of the electrode and the thickness of the  
174 effective dielectric boundary of the interface. A metal that forms  
175 little or no surface oxide, such as platinum, has a dielectric bound-  
176 ary thickness that depends on the thermodynamics of molecules  
177 bouncing off its surface. Metals that form stable nonconductive  
178 oxides, such as tantalum, can be anodized to build up their oxide  
179 thickness, reducing the capacitance but providing a barrier to in-  
180 advertent electrolytic reactions (Guyton and Hambrecht, 1974) and  
181 permitting them to sustain much higher voltages during stimulation  
182 pulses. Other reversible reactions available on some metal surfaces  
183 include absorption and desorption of hydrogen and oxygen. Iridium  
184 provides the highest charge density limit (about  $3 \text{ mC/cm}^2$ ) of any  
185 biocompatible electrode material because it can be "activated" by  
186 growing a multilayer surface oxide that is electrically conductive  
187 and porous to ions (Robblee, Lefko, and Brummer, 1983). Iridium  
188 exhibits a range of stable positive valences from about +3 to +4.8,  
189 so that each atom in the oxide layer can absorb or release about  
190 two electrons, with concomitant release or absorption of two hy-  
191 droxyl ions.

192 Electrochemical considerations are particularly important to at-  
193 tempts to extend neural prosthetic technology to provide denser  
194 multichannel interfaces with the nervous system. In order to pro-  
195 vide more independent channels of stimulation in a given neural  
196 pathway, it is necessary to make the electrodes smaller and position  
197 them closer to their target neurons (Loeb, Peck, and Martyniuk,  
198 1995). Such a microelectrode produces sufficient current density  
199 to activate local neurons selectively, while minimizing the spread  
200 of stimulation current to adjacent sites under the control of other  
201 microelectrodes. Unfortunately, the surface area of such electrodes  
202 tends to decrease faster than the amount of charge required to ac-  
203 tivate local neurons, pushing electrode materials to their safe charge  
204 density limits.

## 205 *Recording*

206 Electrophysiological recordings of interest to the control of neural  
207 prosthetics range from the potentials generated by large populations  
208 of cells (such as those seen in EEG and EMG) to the action poten-

209 tials generated by individual neurons. All of these signals are small-  
210 amplitude AC signals (typically less than 1 mV) that must be de-  
211 tected against a background of interfering signals from other  
212 bioelectrical sources and various sources of noise. In most parts of  
213 the central and peripheral nervous systems, the activity of adjacent  
214 neurons is often quite distinctive, making it necessary to record and  
215 distinguish the action potentials of single units to use them as com-  
216 mand and control signals. This has been accomplished for brief  
217 periods of time in many research applications, but techniques re-  
218 main to be developed for stable, long-term recordings from human  
219 patients.

220 The action potentials generated by individual neurons are pro-  
221 duced by action currents of 1–10 nA lasting 0.2–2 ms, depending  
222 on the size and myelination of the cell. As in the case of the currents  
223 produced by electrical stimulation, the current density and the re-  
224 sulting potential gradient in the surrounding tissues drop rapidly  
225 with distance from the current source (Rall, 1962). Microelectrodes  
226 usually must be within 100  $\mu\text{m}$  of a neuron to record a usable action  
227 potential. In order to be positioned that close to a neuron, such a  
228 microelectrode must be physically small, with a small surface area.  
229 For a metal microelectrode, double-layer charging of the metal-  
230 electrolyte interface provides the mechanism for converting a bio-  
231 potential from ion fluxes in water to electron motion in a metal  
232 conductor. The small surface area of the exposed metal surface  
233 provides only a small capacitance, resulting in a relatively high  
234 impedance in the frequency band of the action potential (typically  
235 100–1,000 k $\Omega$  at 0.5–5 kHz). The resistivity of the saline in the  
236 immediate vicinity of the microelectrode also presents a substantial  
237 impedance. High impedance is associated with high thermal noise,  
238 which adds to and obscures any biopotentials to be recorded.

239 Usually microelectrodes pick up signals from several adjacent  
240 neurons, which may need to be discriminated based on small dif-  
241 ferences in their waveforms. Even relatively low noise levels may  
242 degrade the reliability of such discrimination. Small movements of  
243 the microelectrode with respect to the neurons are likely to distort  
244 the relative amplitude and shape of the single unit potentials or  
245 change the sampled population entirely.

## 246 **Systems Hardware**

### 247 *Power and Data Management*

248 In order to improve the sophistication and capabilities of neural  
249 prosthetic interfaces, larger numbers of stimulating and recording  
250 channels must be positioned closer to their neural targets. This  
251 raises the problem of how to transmit more data to and from arrays  
252 of small electrodes located in delicate neural tissues.

253 One approach is to combine many electrodes into an array that  
254 includes active electronic processing so that a large number of sepa-  
255 rate signals can be multiplexed onto one data connection (Najafi,  
256 Ji, and Wise, 1990). Stimulation pulses are usually relatively brief  
257 ( $\sim 100 \mu\text{s}$ ) compared to their interpulse intervals ( $\sim 10\text{--}100 \text{ms}$ ),  
258 making it possible for a single stimulus channel to be multiplexed  
259 among many electrodes. Bioelectrical potentials are more difficult  
260 to multiplex because they usually have high concurrent bandwidths  
261 (1–10 kHz) on each channel, resulting in very high aggregate sam-  
262 pling rates.

263 Any active circuitry for multiplexing or demultiplexing requires  
264 DC power. Electrical leads and connectors carrying DC voltages are  
265 particularly difficult to insulate because even tiny amounts of saline  
266 leakage result in electrolytic corrosion (see below). The very low  
267 power consumption of some integrated circuit technologies has led  
268 to interest in the wireless transmission of power. Radio-frequency  
269 (RF) inductive coupling is now used routinely in cochlear implants  
270 and has been developed for injectable muscle stimulators (Troyk  
271 and Schwan, 1992). Infrared transmission and photoelectric con-  
272 version may also be possible over short distances.

### 273 *Packaging*

274 Active microelectronic circuitry is generally contained within a  
275 hermetic enclosure to protect it from moisture. This adds greatly  
276 to the physical bulk of the circuitry, particularly if large numbers

277 of input-output channels must be routed through feedthroughs and  
278 connectors incorporated into the package. The design of the pack-  
279 age and the selection of hermetic materials (metals, ceramics, and  
280 glasses) are likely to be further complicated by the need to transmit  
281 RF or infrared energy to power and control the electronics. Em-  
282 bedding in epoxy, silicone, and other nonhermetic polymers was  
283 commonplace in the early cardiac pacemaker industry, but it is  
284 difficult to perform reliably on complex circuits. There is much  
285 interest in passivating monolithic integrated circuits so that they  
286 can be implanted directly into the nervous system with few or no  
287 attached leads.

288 Nonhermetic encapsulation and passivation depends on adhesion  
289 of the coating material to the substrate electronic components rather  
290 than impermeability. Water in the vapor phase tends to diffuse  
291 through all polymeric materials, but it does not cause electronic  
292 problems until it condenses onto the circuitry itself. Once conden-  
293 sation occurs, the water vapor forms an ionic solution by dissolving  
294 surface contaminants or the materials themselves. This solution  
295 represents an osmotic attractant, pulling additional water vapor out  
296 of the surrounding polymer and pressurizing itself so that it dissects  
297 along the surface, eventually bridging electrical conductors and  
298 resulting in corrosion and circuit failure. Condensation on hydro-  
299 philic surfaces can be prevented only if there are no voids and there  
300 is sufficient adhesive force between the encapsulant and all sub-  
301 strate materials. Even trace surface contaminants tend to interfere  
302 with adhesion, which usually depends on electrostatic bonding  
303 (Donaldson, 1987).

304 An alternative approach to chemical adhesion for certain ge-  
305 ometries is to use hydrostatic pressure. This has proved useful in  
306 preventing electrical shorting from condensed water within con-  
307 nectors that must be opened and closed in the body. The encap-  
308 sulant is pressurized mechanically as the connector is closed so that  
309 its hydrostatic pressure exceeds the maximal osmotic pressure of  
310 salt solutions (typically 200–250 psi) (Loeb et al., 1983).

### 311 General Conclusions

312 Serious attempts to build functional neural prostheses have been  
313 under way for about 35 years. Progress has been limited because  
314 it depended on concurrent developments in microelectronic and  
315 biomaterial technologies as well as on advances in understanding  
316 the neurophysiology of the functions to be restored. Once these  
317 thresholds have been passed for a given application (e.g., cochlear  
318 implants for the deaf; see PROSTHETICS, SENSORY SYSTEMS), dra-  
319 matic functional restoration has been achieved, although the de-  
320 velopment of these complex and highly regulated medical devices  
321 remains much slower than that of comparable consumer electron-  
322 ics. As the armamentarium of applicable technology and basic neu-  
323 rophysiology enlarges, there should be a steady acceleration in the  
324 clinical application of neural prostheses.

325 **Roadmap:** Applications

326 **Related Reading:** Brain-Computer Interfaces; Brain Signal Analysis; Pros-  
327 thetics, Motor Control; Prosthetics, Sensory Systems

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359 **AQ 1: Au: “such as measured by EEG and EEG”?**  
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